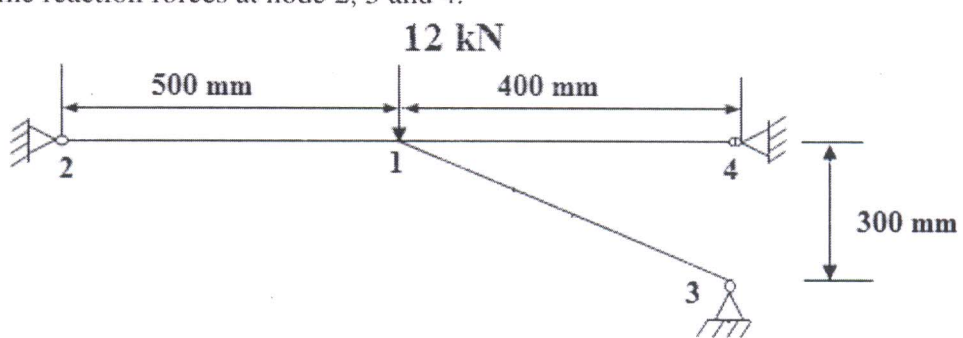


Total No of Questions: [12]		SEAT NO. : <div></div>	
[Total No. of Pages : 6]			
B.E. Mechanical (2008 Pattern)			
Finite Element Method			
(Elective - III) (Semester - II)			
Time: 3 Hours		Max. Marks : 100	
Instructions to the candidates:			
1) Answers to the two sections should be written in separate answer books.			
2) Neat diagrams must be drawn wherever necessary.			
3) Figures to the right side indicate full marks.			
4) Use of Calculator is allowed.			
5) Assume Suitable data if necessary.			
6) Additional data sheet is attached for the reference.			
SECTION I			
Unit I			
Q1)	a)	Explain how banded skyline solution method is used to solve simultaneous equations.	[8]
	b)	List at least 6 advantages of Finite Element Method over analytical method. Also list disadvantages or limitations of FEM.	[8]
OR			
Q2)	a)	Explain the terms essential and natural boundary conditions. Give example of each.	[8]
	b)	Explain in detail the method of matrix partitioning and how it is used to impose boundary conditions in finite element method.	[8]
Unit II			
Q3)	a.)	For the plane truss shown in Figure 3a, determine the following. Each element has $E = 70 \text{ GPa}$, and area $A = 200 \text{ mm}^2$. i. write down the elemental stiffness matrices (k) for each element, ii. assemble k matrices to get global stiffness matrix (K), iii. apply boundary conditions, iv. find horizontal and vertical displacements of node 1, v. determine reaction forces at node 2, 3 and 4.	[10]
			
Figure 3a			
	b)	For the five spring assemblage shown in Figure 3b, determine the displacements at nodes 2 and 3 and the reactions at nodes 1 and 4. Assume the rigid vertical bars at nodes 2 and 3 connecting the springs remain horizontal at all times but are free to slide or displace left or right. There is an applied force at node 3 of 1000 N to the right. Consider $k_1 = 500\text{N/mm}$, $k_2 = k_3 = 300\text{N/mm}$, and $k_4 = k_5 = 400\text{N/mm}$	[8]

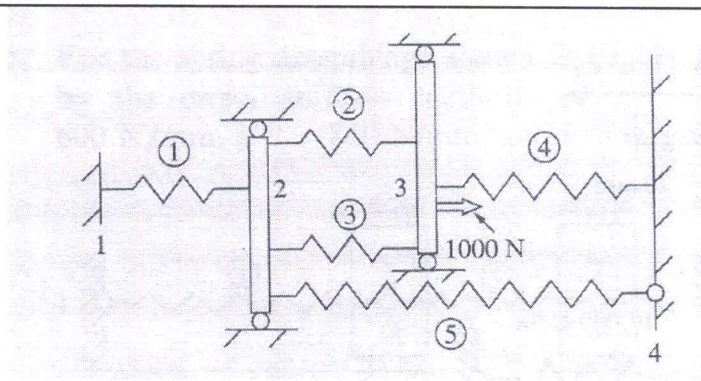


Figure 3b

OR

Q4)	a)	Derive elemental stiffness matrix and force vector for two-noded (linear) bar element using Principle of Minimum Potential Energy (PMPE) Method. The bar element is oriented in x-direction. Assume that only concentrated forces are acting on the nodes of bar element. Ignore surface tractions and the body forces.	[10]
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	b)	For the beam shown in Figure 4b, determine the displacements and the slope at node 2. Also find the reaction forces and moments at nodes 1 and 3. Consider $E = 210 \text{ GPa}$, and $I = 4 \times 10^{-4} \text{ m}^4$	[8]
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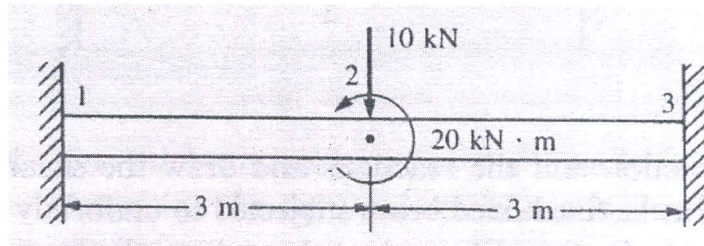


Figure 4b

Unit III

Q5)		Evaluate the following integrals.	
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	a)	use two-point Gaussian quadrature method	[5]
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$$I = \int_0^1 \frac{1}{1+x^2} dx$$

	b)	use two-point Gaussian quadrature method	[5]
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$$I = \int_1^5 [3^x + 1] dx$$

	c)	use three-point Gaussian quadrature method	[6]
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$$I = \int_4^5 \frac{2 \sin(x)}{x^2} dx$$

OR

Q6)	a)	Explain with neat sketches the difference between p and h refinements in Finite Element Method.	[6]
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- b) For the three-noded iso-parametric bar element shown in Figure 6b, show that the Jacobean determinate is $|J| = L/2$. Also determine the shape functions $N1 - N3$ and the strain-displacement matrix $[B]$. Assume the displacement field as $u = a1 + a2s + a3s^2$. [10]

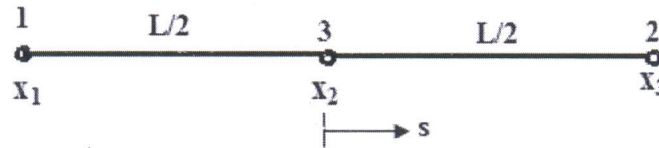


Figure 6b

SECTION II

Unit IV

- Q7) Determine the temperature distribution along the length of the rod (at $L/4$, $L/2$, $3L/4$, and L) as shown in Figure 7. The rod with radius of 25 mm is insulated at the perimeter. The left end has a constant temperature of 40°C and a free stream temperature T_∞ is -10°C . Let $K_{xx} = 35 \text{ W/(m}^\circ\text{C)}$ and $h = 55 \text{ W/(m}^2\text{ }^\circ\text{C)}$. [16]

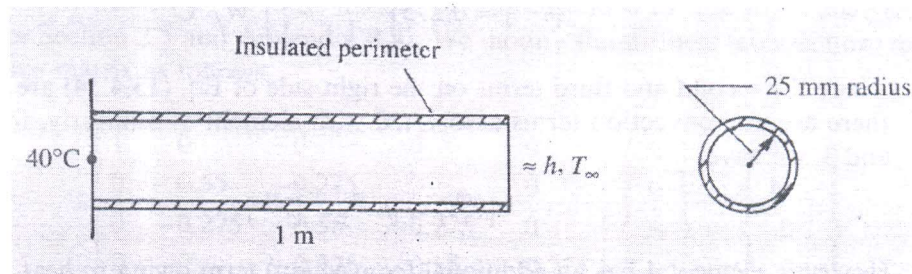


Figure 7

OR

- Q8) A composite wall shown in Figure 8 is composed of two homogeneous slabs in contact. Let thermal conductivities be $K1 = 1 \text{ W/(m}^\circ\text{C)}$ for firebrick slab 1 and $K2 = 0.3 \text{ W/(m}^\circ\text{C)}$ for insulating slab 2. The left side is exposed to an ambient temperature of $T_{\infty L} = 1000^\circ\text{C}$ inside the furnace with heat transfer coefficient of $hL = 10 \text{ W/(m}^2\text{ }^\circ\text{C)}$. The right side ambient temperature is $T_{\infty R} = 25^\circ\text{C}$ outside of the furnace with heat transfer coefficient of $hR = 3 \text{ W/(m}^2\text{ }^\circ\text{C)}$. The thicknesses of the slabs are $L1 = 0.20 \text{ m}$, and $L2 = 0.10 \text{ m}$. Determine the temperature at the left edge, point between the two slabs and right edge of the composite wall. [16]

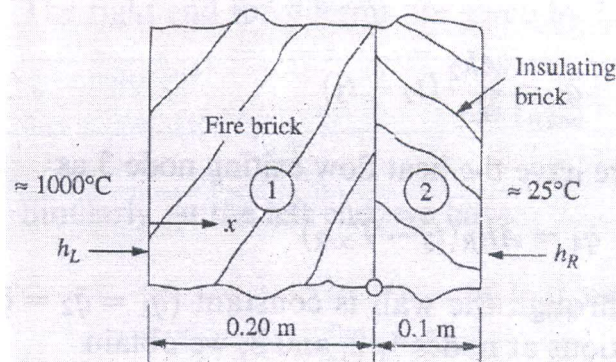
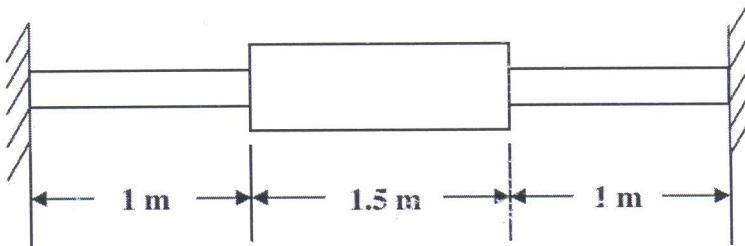


Figure 8

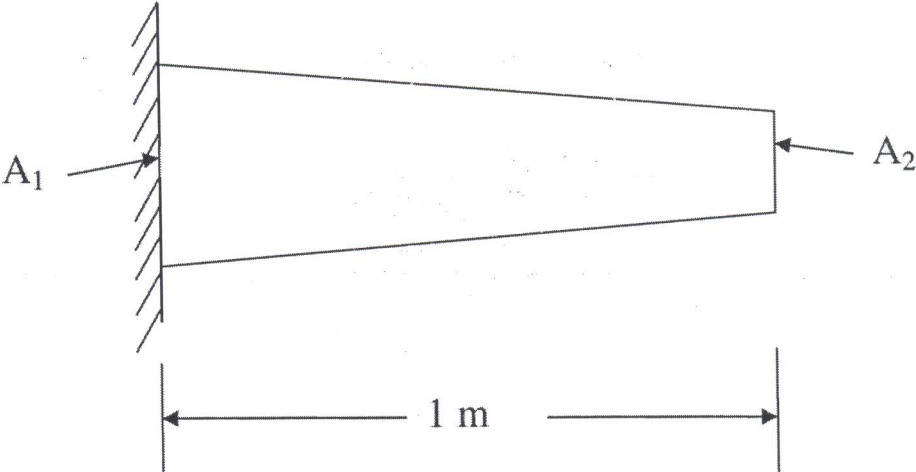
Unit V

Q9)	a)	For the stepped bar shown in Figure 9a, determine the first two natural frequencies in terms of rad/s for un-damped free vibration. Let $A_1 = A_3 = 5 \text{ cm}^2$, $A_2 = 10 \text{ cm}^2$, $E = 210 \text{ GPa}$, and $\rho = 7860 \text{ kg/m}^3$. Use consistent mass matrices for each element.	[12]
			
Figure 9a			

b) Explain eigenvalue problem for un-damped free vibration system

[6]

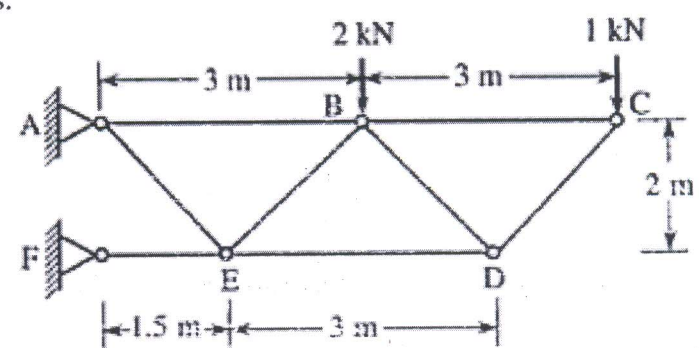
OR

Q10)	a)	For the tapered beam with square cross sectional area shown in Figure 10, set-up the problem to find characteristic equation to determine first four natural frequencies. Consider two elements of average cross sectional area and equal lengths. Each element has $E = 200 \text{ GPa}$, density $\rho = 7500 \text{ kg/m}^3$, $A_1 = 9 \text{ cm}^2$, and $A_2 = 4 \text{ cm}^2$. Use consistent mass matrix.	[18]
			
Figure 10			

Unit VI

Q11)	a)	What are various meshing techniques?	[8]
	b)	Explain the terms strain and stress recovery in post-processing stage.	[8]

OR

Q12)		Consider the truss problem shown in Figure 12 for the calculation of displacements. For this problem write down nodal coordinates, element connectivity, type of analysis, loading and boundary conditions.	[16]
			
Figure 12			

DATA SHEET

Shape Functions:

1 Bar Element:

$$N_1 = 1 - \frac{x}{L} \quad N_2 = \frac{x}{L}$$

2 Beam Element:

$$N_1 = \frac{1}{L^3}(2x^3 - 3x^2L + L^3)$$

$$N_2 = \frac{1}{L^3}(x^3L - 2x^2L^2 + xL^3)$$

$$N_3 = \frac{1}{L^3}(-2x^3 + 3x^2L)$$

$$N_4 = \frac{1}{L^3}(x^3L - x^2L^2)$$

Elemental Stiffness Matrices:

1 Bar Element:

$$k_{bar} = \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

2 Beam Element:

$$k_{beam} = \frac{EI}{L^3} \begin{bmatrix} 12 & 6L & -12 & 6L \\ 6L & 4L^2 & -6L & 2L^2 \\ -12 & -6L & 12 & -6L \\ 6L & 2L^2 & -6L & 4L^2 \end{bmatrix}$$

3 Truss Element:

$C = \cos(\theta)$ and $S = \sin(\theta)$

θ is positive in anti clockwise direction.

$$k_{truss} = \frac{AE}{L} \begin{bmatrix} C^2 & CS & -C^2 & -CS \\ CS & S^2 & -CS & -S^2 \\ -C^2 & -CS & C^2 & CS \\ -CS & -S^2 & CS & S^2 \end{bmatrix}$$

Elemental Mass Matrices:

1 Bar Element:

(a) Consistent mass matrix:

$$m_{consistent} = \frac{\rho AL}{6} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix}$$

	(b)	Lumped mass matrix:																
		$m_{lumped} = \frac{\rho AL}{2} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$																
	2	Beam Element:																
	(a)	Consistent mass matrix:																
		$m_{consistent} = \frac{\rho AL}{420} \begin{bmatrix} 156 & 22L & 54 & -13L \\ 22L & 4L^2 & 13L & -3L^2 \\ 54 & 13L & 156 & -22L \\ -13L & -3L^2 & -22L & 4L^2 \end{bmatrix}$																
	(b)	Lumped mass matrix:																
		$m_{lumped} = \frac{\rho AL}{2} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$																
Heat Transfer Matrices:																		
		k matrix for Conduction + Convection for bar element:																
		$k = \frac{AK}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} + \frac{hPL}{6} \begin{bmatrix} 2 & 1 \\ 1 & 2 \end{bmatrix}$																
		where, A = cross sectional area, K = Thermal Conductivity, L = Length of an element, h = Convection Coefficient, and P = Perimeter.																
Gauss Quadrature:																		
		Table for Gauss Points for integration from -1 to 1																
		$\int_{-1}^1 y(x)dx = \sum_{i=1}^n W_i y_i$																
		<table><tr><th>Number of Points</th><th>Locations, x_i</th><th>Associated Weights, W_i</th></tr><tr><td>1</td><td>$x_1 = 0.000$</td><td>2.000</td></tr><tr><td>2</td><td>$x_1, x_2 = \pm 0.57735$</td><td>1.000</td></tr><tr><td>3</td><td>$x_1, x_3 = \pm 0.77459$ $x_2 = 0.000$</td><td>$5/9 = 0.55556$ $8/9 = 0.88889$</td></tr><tr><td>4</td><td>$x_1, x_4 = \pm 0.86113$ $x_2, x_3 = \pm 0.33998$</td><td>0.34785 0.65214</td></tr></table>	Number of Points	Locations, x_i	Associated Weights, W_i	1	$x_1 = 0.000$	2.000	2	$x_1, x_2 = \pm 0.57735$	1.000	3	$x_1, x_3 = \pm 0.77459$ $x_2 = 0.000$	$5/9 = 0.55556$ $8/9 = 0.88889$	4	$x_1, x_4 = \pm 0.86113$ $x_2, x_3 = \pm 0.33998$	0.34785 0.65214	
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