

Paper Code - U19-102 (T1)

OCTOBER 2019 / IN-SEM (T1)

F. Y. B.TECH. (COMMON) (SEMESTER - I)

COURSE NAME: BASIC ELECTRICAL ENGINEERING

COURSE CODE: ET 10182A

MODEL ANSWER AND MARKING SCHEME

(PATTERN 2018)

Time: [1 Hour]

[Max. Marks: 20]

(*) Instructions to candidates:

- 1) All questions are compulsory.
- 2) Figures to the right indicate full marks.
- 3) Use of scientific calculator is allowed.
- 4) Use suitable data where ever required.
- 5) Assume suitable data, if required.

Q 1) Attempt any two.

- a) Current through 3Ω resistance can be found using Superposition theorem

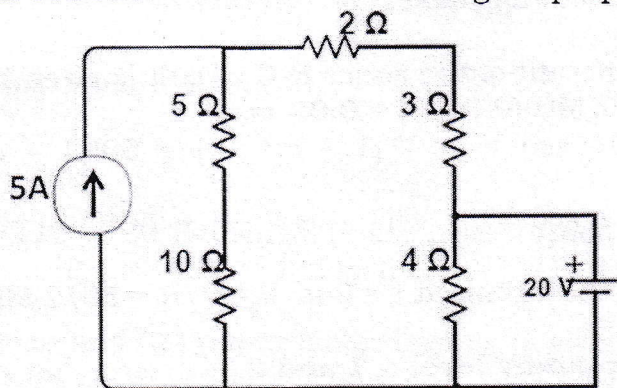


Fig. 1

Considering 5A current source acting alone. 20 V voltage source is shorted.

Applying current division rule,

$$I_{3\Omega}' \text{ (5 A current source alone)} = (5 \times 15) / (15 + 2 + 3) = \mathbf{3.75 \text{ A}} \text{ downwards } \mathbf{1M}$$

Considering 20 V voltage source acting alone. 5A current source is open circuited.

Total current delivered by 20 V voltage source is

$$I_T = (20) / [(10 + 5 + 2 + 3) \parallel (4)] = 20 \times 24 / 80 = 6 \text{ A}$$

Applying current division rule,

$$I_{3\Omega}' \text{ (20 V voltage source alone)} = (6 \times 4) / (10 + 5 + 2 + 3 + 4) = \mathbf{1 \text{ A}} \text{ upwards } \mathbf{2M}$$

Total current through 3Ω resistance is given as

$$I_{3\Omega} = I_{3\Omega}' \text{ (5 A current source alone)} + I_{3\Omega}' \text{ (20 V voltage source alone)}$$

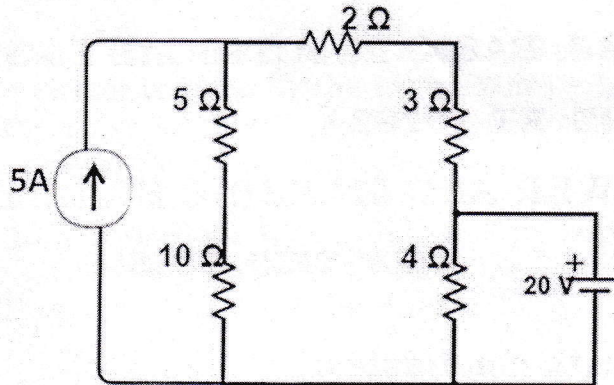
$$= 3.75 - 1 = \mathbf{2.75 \text{ A}}$$

1M

Bloom's Taxonomy level :- 3

CO:- 1

- b) Removing the load branch of 3Ω resistance



Applying KVL to loop

$$-20 + 4I = 0 \quad 4I = 20$$

$$\text{Therefore, } I = 5 \text{ A}$$

1M

$$V_{Th} = V_{oc} = 2(0) + (5+10)(5) - 4(5) = \mathbf{55 \text{ V}}$$

1M

$$R_{eq} = 2 + 5 + 10 + (4 \parallel 0) = 17 + 0 = \mathbf{17 \Omega}$$

1M

Drawing Thevenin's equivalent circuit with correct V_{Th} and R_{eq} .

1M

Bloom's Taxonomy level :- 3

CO;- 1

- c) The time constant of the series R-C circuit is given by

$$\zeta = RC = (2 \text{ M}\Omega)(0.01 \mu\text{F}) = \mathbf{0.02 \text{ sec}}$$

1M

$$\text{At } t = 0.01 \text{ sec } V_c = V*[1 - e^{(-t/\zeta)}] = 50*[1 - e^{(-0.01/0.02)}] = \mathbf{30.32 \text{ V}}$$

1M

$$\text{At } t = 0.02 \text{ sec } V_c = V*[1 - e^{(-t/\zeta)}] = 50*[1 - e^{(-0.02/0.02)}] = \mathbf{31.606 \text{ V}}$$

1M

$$\text{Current in the circuit at } t = 0 \text{ is } I_0 = V/R = 50/2 \text{ M}\Omega = \mathbf{25 \mu\text{A}}$$

1M

Bloom's Taxonomy level :- 1 and 2

CO;- 1

Q 2) Attempt any **two**.

- a) $v = V_m \sin \omega t$ Volt and $i = I_m \sin(\omega t + \Phi)$ Amp

$$\text{Instantaneous power, } p = v*i = (V_m \sin \omega t) * [I_m \sin(\omega t + \Phi)]$$

$$= V_m I_m \sin \omega t \sin(\omega t + \Phi)$$

$$\text{Using } \cos(A - B) - \cos(A + B) = 2 \sin A \sin B$$

$$p = (V_m I_m / 2) * [\cos(\omega t - \omega t + \Phi) - \cos(2\omega t + \Phi)]$$

$$p = (V_m I_m / 2) * [\cos \Phi - \cos(2\omega t + \Phi)]$$

Integrating this instantaneous power over a cycle, the average power in the circuit is given by,

$$\mathbf{P_{av} = (V_m I_m / 2) \cos \Phi = V I \cos \Phi \text{ W}}$$

4M

Bloom's Taxonomy level :- 2 and 3

CO;- 2

b) Apparent power $S = 10 \text{ KVA}$ $Q = 8 \text{ KVAR}$
 Power consumed, $P = \sqrt{[(S)^2 - (Q)^2]} = \sqrt{(100 - 64)} = 6 \text{ KW}$
1M
 $\sin \Phi = 8/10 = 0.8$ $\cos \Phi = 0.6$
 Power consumed, $P = V I \cos \Phi$
 $6000 = 230 * I * 0.6$
 $I = 6000 / (230 * 0.6) = 43.47 \text{ A}$ **1M**
 $Z = V/I = 230/43.47 = 5.2910 \Omega$
 $R = Z \cos \Phi = 5.2910 * 0.6 = 3.1746 \Omega$ **1M**
 $X_L = Z \sin \Phi = 5.2910 * 0.8 = 4.2328 \Omega$
 $L = X_L / 2 * \pi * f = 4.2328 / 2 * \pi * 50 = 0.01347 \text{ H} = 13.47 \text{ mH}$ **1M**

Bloom's Taxonomy level :- 4

CO;- 2

c) $R = 10 \Omega$ $L = 0.1 \text{ H}$ $C = 150 \mu\text{F}$ $V = 200 \text{ V}$ $f = 50 \text{ Hz}$
 $X_L = \omega L = 2 * \pi * f * L = 2 * \pi * 50 * 0.1 = 31.41 \Omega$
 $X_C = 1/\omega C = 1/ 2 * \pi * f * C = 1/2 * \pi * 50 * 150 * 10^{-6} = 21.22 \Omega$
 $Z = R + j X_L - j X_C = 10 + j(X_L - X_C) = 10 + j(31.41 - 21.22) = 10 + j10.19$
 $= 14.27 \angle 45.53^\circ \Omega$ **1M**
 $I = V/Z = 200/14.27 \angle 45.53^\circ = 14.01 \text{ A}$ **1M**
 $\cos \Phi = \cos 45.53^\circ = 0.7 \text{ lag}$
 $P = V I \cos \Phi = 200 * 14.01 * 0.7 = 1.96 \text{ kW}$ **1M**
 Frequency at which circuit will undergo resonance is given by,
 $f = 1/2 * \pi * \sqrt{L * C} = 1/2 * \pi * \sqrt{0.1 * 150 * 10^{-6}} = 41.09 \text{ Hz}$ **1M**

Bloom's Taxonomy level :- 2 and 3

CO;- 2

Q 3) Attempt any **one**.

- a) A 1.5 KVA, 220/110 V, 50 Hz, single phase transformer
 $P_{\text{core}} = 32 \text{ W}$ $P_{\text{cu}} = 44 \text{ W}$ at full load

efficiency at full load and 0.8 power factor lagging is given as,

$$\eta = [(KVA * 1000 * \cos \Phi) / (KVA * 1000 * \cos \Phi) + P_{\text{core}} + P_{\text{cu}}] * 100$$

$$= [1500 * 0.8 / 1500 * 0.8 + 32 + 44] = 94.04 \% \quad \text{2M}$$

efficiency at half load and unity power factor is given as,

$$\eta = [(KVA * 1000 * \cos \Phi) / (KVA * 1000 * \cos \Phi) + P_{\text{core}} + \frac{1}{4} * P_{\text{cu}}] * 100$$

$$= [1500 * 1 / 1500 * 1 + 32 + 11] * 100$$

$$= 97.21 \% \quad \text{2M}$$

Bloom's Taxonomy level :- 1 and 2

CO;- 3

- b) Let N_1 = No. of turns on primary winding
 N_2 = No. of turns on secondary winding
 E_1 = rms value of emf induced in primary winding
 E_2 = rms value of emf induced in secondary winding

Φ_m = maximum flux in the core

f = frequency of the supply

Let $\Phi = \Phi_m \sin \omega t$ be flux in the core

According to Faraday's laws of electromagnetic induction emf induced in primary winding is,

$$e_1 = -N_1 d\Phi/dt = -N_1 d/dt \{\Phi_m \sin \omega t\} = -N_1 \omega \Phi_m \cos \omega t \\ = -N_1 d\Phi/dt = -N_1 d/dt \{\Phi_m \sin \omega t\} = N_1 \omega \Phi_m \sin(\omega t - \pi/2)$$

rms value of emf induced in primary winding is given by,

$$E_1 = N_1 \omega \Phi_m / \sqrt{2} = N_1 * 2 * \pi * f * \Phi_m / \sqrt{2} = \mathbf{4.44f\Phi_m N_1 \text{ Volts}} \quad \mathbf{2M}$$

emf induced in secondary winding is,

$$e_2 = -N_2 d\Phi/dt = -N_2 d/dt \{\Phi_m \sin \omega t\} = -N_2 \omega \Phi_m \cos \omega t \\ = -N_2 d\Phi/dt = -N_2 d/dt \{\Phi_m \sin \omega t\} = N_2 \omega \Phi_m \sin(\omega t - \pi/2)$$

Similarly rms value of emf induced in secondary winding by Faraday's laws is given by,

$$E_2 = N_2 \omega \Phi_m / \sqrt{2} = N_2 * 2 * \pi * f * \Phi_m / \sqrt{2} = \mathbf{4.44f\Phi_m N_2 \text{ Volts}} \quad \mathbf{2M}$$

OR

Let N_1 = No. of turns on primary winding

N_2 = No. of turns on secondary winding

E_1 = rms value of emf induced in primary winding

E_2 = rms value of emf induced in secondary winding

Φ_m = maximum flux in the core

f = frequency of the supply

Let $\Phi = \Phi_m \sin \omega t$ be flux in the core

According to Faraday's laws of electromagnetic induction average value of emf induced per turn considering first quarter cycle is,

$$e = d\Phi/dt = (\Phi_m - 0) / (T/4) = 4\Phi_m f$$

For sinusoidal waveform, form factor which is equal to rms value/average value is 1.11 Hence, rms value of emf induced per turn is,

$$E = 1.11 * 4\Phi_m f = 4.44f\Phi_m \quad \mathbf{2M}$$

rms value of emf induced in primary winding is given by,

$$E_1 = \mathbf{4.44f\Phi_m N_1 \text{ Volts}} \quad \mathbf{1M}$$

rms value of emf induced in secondary winding is given by,

$$E_2 = \mathbf{4.44f\Phi_m N_2 \text{ Volts}} \quad \mathbf{1M}$$

Bloom's Taxonomy level :- 3

CO₃:- 3