

or code:

119-114(T1)

Marking Scheme

R.S. Apte

T-1, FEA, CVPB11184A

FYM. Tech (Structures)

(2018 KI-pattern)

Q1 Δ_1, Δ_2 at A $\begin{matrix} \uparrow 2 \\ \rightarrow 1 \end{matrix}$ ----- (2 marks)

$$[K][\Delta] = [P], \theta = 36.86^\circ \text{ --- (1 mark)}$$

$$K_{11} = \sum \frac{AE}{L} \cos^2 \theta = 1012, K_{22} = \sum \frac{AE}{L} \sin^2 \theta = 288$$

$$K_{12} = K_{21} = \frac{AE}{L} \sin \theta \cos \theta = 384 \text{ --- (4 marks)}$$

$$\begin{bmatrix} 1012 & 384 \\ 384 & 288 \end{bmatrix} \begin{bmatrix} \Delta_1 \\ \Delta_2 \end{bmatrix} = \begin{bmatrix} 0 \\ -200 \end{bmatrix}, \Delta_1 = 0.534, \Delta_2 = -1.406 \text{ --- (2 marks)}$$

$$F_{AB} = 267 \text{ kN (T)}, P_{AC} = -333.410 \text{ kN (comp)} \text{ --- (1 mark)}$$

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Q2 @ Expression $\epsilon_x = \frac{\sigma_x}{E} - \mu \frac{\sigma_y}{E} - \mu \frac{\sigma_z}{E}, \epsilon_y, \epsilon_z, \text{ --- (1 mark)}$

$$\gamma_{xy} = \tau_{xy}/G, \gamma_{yz} = \tau_{yz}/G, \gamma_{zx} = \tau_{zx}/G.$$

$$G = E/2(1+\mu)$$

--- (2) mark

$$\epsilon_x = \frac{\sigma_x}{E} - \mu \frac{\sigma_y}{E} - \mu \frac{\sigma_z}{E} + 0 \tau_{xy} + 0 \tau_{yz} + 0 \tau_{zx} \text{ --- (1)}$$

$$\epsilon_y = -\mu \frac{\sigma_x}{E} + \frac{\sigma_y}{E} - \mu \frac{\sigma_z}{E} + 0 \tau_{xy} + 0 \tau_{yz} + 0 \tau_{zx} \text{ --- (1)}$$

similarly, $\epsilon_z, \gamma_{xy}, \gamma_{yz}, \gamma_{zx}$

matrix form $\begin{Bmatrix} \epsilon \end{Bmatrix} = \begin{Bmatrix} 6 \times 6 \end{Bmatrix} \begin{Bmatrix} \sigma \end{Bmatrix}, \sigma = [c] \epsilon \text{ --- (1)}$

6x1 6x1

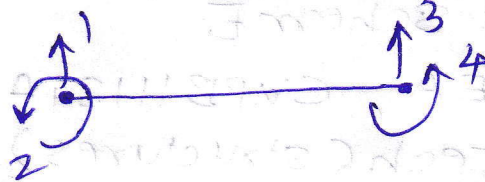
$$\begin{Bmatrix} \sigma \end{Bmatrix} = \begin{Bmatrix} D \end{Bmatrix} \begin{Bmatrix} \epsilon \end{Bmatrix} \text{ --- (1)}$$

↑ strain-stress ↑ elastic coefficient

06.

(b) Advantages - (2), Disadvantages - (2) = 04

Q3 (a)



$$\begin{bmatrix} K_{11} = 12EI/L^3 \\ K_{21} = 6EI/L^2 \\ K_{31} = -12EI/L^3 \\ K_{41} = 6EI/L^2 \end{bmatrix} \quad \text{--- (2 marks)}$$

$$K_{12} = 6EI/L^2, \quad K_{32} = -6EI/L^2$$

$$K_{22} = 4EI/L, \quad K_{42} = 2EI/L$$

$$\begin{bmatrix} K_{13} = -12EI/L^3 \\ K_{23} = -6EI/L^2 \\ K_{33} = 12EI/L^3 \\ K_{43} = -6EI/L^2 \end{bmatrix}$$

$$K_{14} = 6EI/L^2, \quad K_{24} = 2EI/L, \quad K_{34} = -6EI/L^2, \quad K_{44} = 4EI/L$$

$$[K] = \frac{EI}{L^3} \begin{bmatrix} 12 & 6L & -12 & 6L \\ 6L & 4L^2 & -6L & 2L^2 \\ -12 & -6L & 12 & -6L \\ 6L & 2L^2 & -6L & 4L^2 \end{bmatrix} \quad \text{--- (1 mark)}$$

06

Q3 (b) 1D, 2D, 3D elements, with nodes --- (1+1+1+1)
↑ nodes

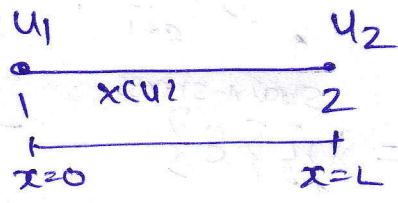
Q4 (a). Field variable at any point in element related to nodal points of element

$$\{\delta\} = \{N\} \{\delta\} \quad \text{--- (1)}$$

$\uparrow$ shape function $\uparrow$ nodal displacement
 $\uparrow$ within element example.

- ① Easy to handle,
 - ② Approximated reasonably well
- (2 marks)

4(b).



$$u = \alpha_1 + \alpha_2 x \quad \text{--- (1 mark)}$$

At 1, $x=0, u=u_1$
 At 2, $x=L, u=u_2$

$$u_1 = \alpha_1, \quad u_2 = \alpha_1 + \alpha_2 L, \quad \alpha_2 = \frac{u_2 - u_1}{L} \quad \text{--- (1 mark)}$$

$$u = u_1 + \left(\frac{u_2 - u_1}{L} \right) x$$

$$u = \frac{u_1 \times L + u_2 x - u_1 x}{L} = \frac{u_1 (L - x)}{L} + \frac{u_2 x}{L} \quad \text{--- (1 mark)}$$

$$u = \underline{u_1} \left(1 - \frac{x}{L} \right) + \left(\frac{x}{L} \right) u_2$$

$$u = N_1 u_1 + N_2 u_2$$

$N_1 = 1 - x/L, \quad N_2 = x/L$ - shape function --- (1 mark)