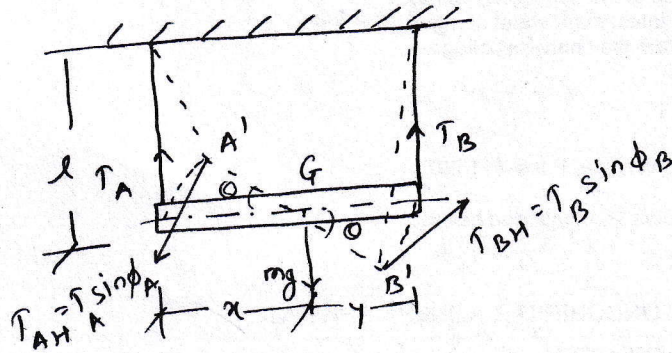


T. X. B. Tech (Mechanical)

Course:- Dynamics of Machinery
MEVA31172

Q1] a] Bifilar suspension:- (6 marks)



m = mass of rigid body
 k = radius of gyration @ G.
 l = length of each string
 y = distance of A from G
 x = distance of B from G
 α = angular accelⁿ of rigid body.

Taking moment at 'A'

— 1 marks

$$T_B(x+y) = mgx \therefore T_B = \frac{mgx}{x+y} \quad \text{--- (A)}$$

Taking moment at 'B'

$$T_A(x+y) = mgy \therefore T_A = \frac{mgy}{x+y} \quad \text{--- (B)}$$

Body displaced from eqm position through ' θ '

$$AA' = x\theta = \phi_A l \quad \phi_A = \frac{\theta x}{l} \quad \text{--- (C)}$$

$$BB' = y\theta = \phi_B l \quad \phi_B = \frac{\theta y}{l} \quad \text{--- (D)} \quad \text{--- 1 marks}$$

The component of tension ' T_A ' in horizontal plane

$$\sin \phi_A = \frac{T_{AH}}{T_A} \quad T_{AH} = T_A \sin \phi_A = T_A \phi_A \quad \text{--- (E)}$$

$$T_{BH} = T_B \phi_B \quad \text{--- (F)} \quad \text{--- 1 marks}$$

putting (B) & (C) in (E)

$$T_{AH} = \frac{mgxy\omega}{l(x+y)} - (G)$$

putting (A) & (D) in (F)

$$T_{BH} = \frac{mgxy\omega}{l(x+y)} - (H)$$

so,

$$T = T_{AH} \times x + T_{BH} \times y$$

$$T = \frac{mgxy\omega}{l(x+y)} \times x + \frac{mgxy\omega}{l(x+y)} \times y$$

$$T = \frac{mgxy\omega}{l} - (I) \quad \text{--- } \underline{\underline{2 \text{ marks}}}$$

'angular accel' of connecting rod.

$$T = I_G \cdot \alpha$$

$$T = mk^2 \alpha \quad \therefore \frac{mgxy\omega}{l} = mk^2 \alpha$$

$$\frac{\alpha}{\omega} = \frac{gxy}{lk^2}$$

$$\therefore f_n = \frac{1}{2\pi} \sqrt{\frac{\text{angular accel}^n}{\text{angular dis}^m}}$$

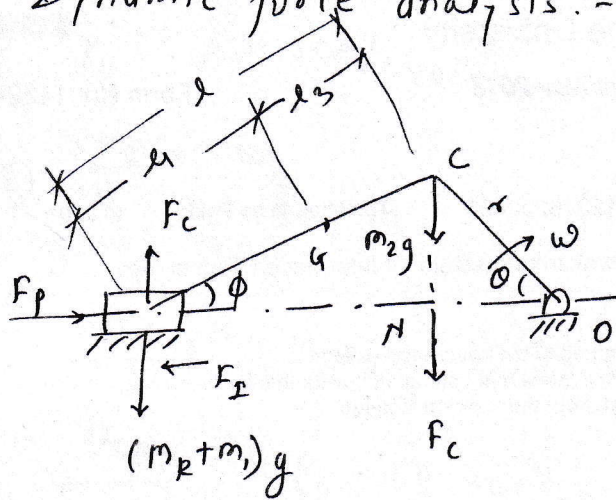
$$= \frac{1}{2\pi} \sqrt{\frac{gxy}{lk^2}}$$

$$\boxed{f_n = \frac{1}{2\pi k} \sqrt{\frac{gxy}{l}}} \quad \text{cycle/sec or Hz}$$

--- 1 mark

--- x o x --- x o x --- x o x ---

Q2] a] Dynamic force analysis:- (6 marks)



— 2 marks

a) Torque exerted on crank shaft due to inertia force (T_1)

$$T_1 = F_p r \left[\sin \theta + \frac{\sin 2\theta}{2\sqrt{n^2 - \sin^2 \theta}} \right]$$

— 1 marks

b) Torque exerted on crank shaft due to correction couple (T_2)

$$T_2 = -m_c (k_1^2 - k^2) \alpha \frac{\cos \theta}{\sqrt{n^2 - \sin^2 \theta}} \quad \underline{\underline{1 \text{ mark}}}$$

c) Torque exerted on crank shaft due to mass m_2 (T_3)

$$T_3 = (m_2 g) r \sin \theta \quad \underline{\underline{1 \text{ mark}}}$$

(4) Total torque:-

$$T = T_1 + T_2 + T_3 \quad \underline{\underline{1 \text{ mark}}}$$

b] connecting rod:- $\overline{\text{X O X}} \quad \overline{\text{X O X}} \quad \overline{\text{X O X}} \quad \underline{\underline{(6 \text{ marks})}} \quad \underline{\underline{1 \text{ mark}}}$
 $l_1 = 0.15 \text{ m}, \quad l_2 = 0.0666 \text{ m}$

$$m_1 = 0.6149 \text{ kg}, \quad m_2 = 1.3846 \text{ kg} \quad \underline{\underline{2 \text{ marks}}}$$

$$T_c = -1.97795 \text{ N-m (anticlockwise)} \quad \underline{\underline{3 \text{ marks}}}$$

b] step 1:- (6 marks)

① $t_p = 3.5 \text{ sec/cycle}$

step 2:-

② $k_1 = 0.1950 \text{ m}$

1 mark

step 3:-

③ $I_{G_1} = 0.05707 \text{ kg m}^2$

1 mark

step 4:-

④ $t_p = 3 \text{ sec/cycle}$

7 mark

step 5:-

⑤ $k = 0.1671 \text{ m}$

1 mark

step 6:-

⑥ $I_{G_2} = 0.1817 \text{ kg m}^2$

1 mark

step 7:-

⑦ $I_{G_2} = 0.1246 \text{ kg m}^2$

1 mark

--- xox --- xox --- xox ---

c] concept of Equivalent length of Simple pendulum:- (4 marks)

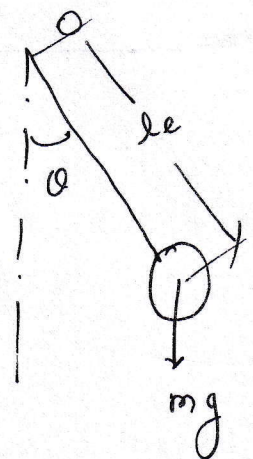
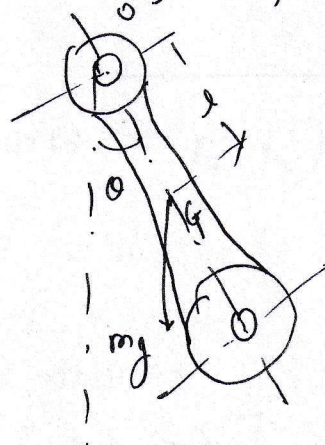
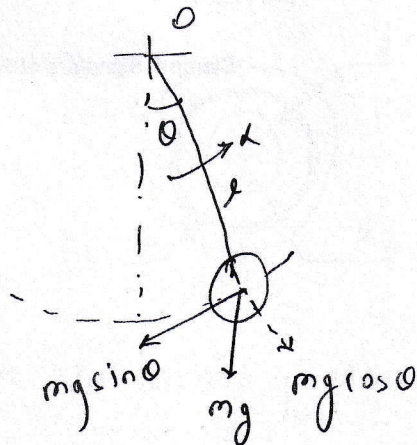


Fig - 2 marks

length of equivalent length

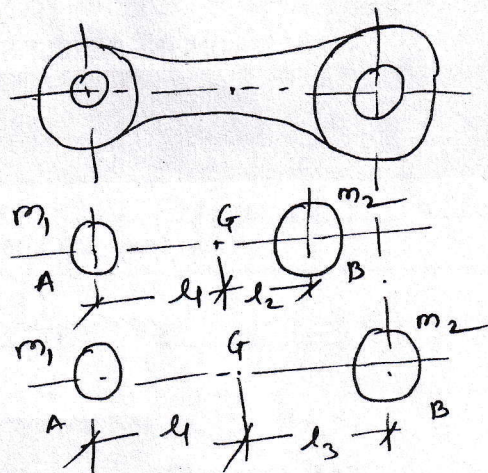
$$\therefore l_e = \frac{k^2 + l^2}{l}$$

$$= \frac{k^2}{l} + l$$

2 marks

c] - correction couple:- (4 marks).

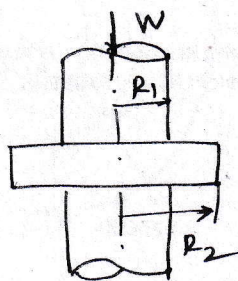
Fig. with
explanation
2 marks



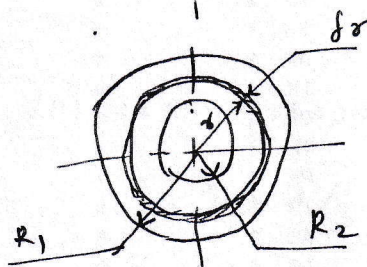
$$T_c = m l_1 (l_3 - l_2) \times \text{---} \underline{\underline{2 \text{ marks}}}$$

--- x o x --- x o x --- x o x ---

Q3] a] Flat collar thrust bearing:- (6 marks)



--- Fig - 2 marks



$$\text{area} = \pi (R_1^2 - R_2^2)$$

* Uniform pressure theory

$$T = \frac{2}{3} \mu W \left[\frac{R_1^3 - R_2^3}{R_1^2 - R_2^2} \right] \text{---} \underline{\underline{2 \text{ marks}}}$$

* Uniform wear theory

$$T = \frac{1}{2} \mu W (R_1 + R_2) \text{---} \underline{\underline{2 \text{ marks}}}$$

--- x o x --- x o x --- x o x ---

b] For $2\theta = 30^\circ$ $p = 350 \text{ N}$ --- 2 marks

For $2\theta = 90^\circ$ $p = 319.69 \text{ N}$ --- 2 marks

c] * self-locking of brakes:- ($\alpha \leq \mu \cdot a$) - (4 marks)

$$R_n = \frac{Pl}{\alpha - \mu \cdot a}$$

$$p = \frac{R_n (\alpha - \mu \cdot a)}{l}$$

— 2 marks

* self-energizing :- ($p > 0$)

$$p = \frac{R_n (\alpha - \mu \cdot a)}{l}$$

$$R_n \cdot \alpha = Pl + \mu R_n \cdot a$$

— 2 marks

Q4] a] Torque expression of "cone clutch":- (6 marks)

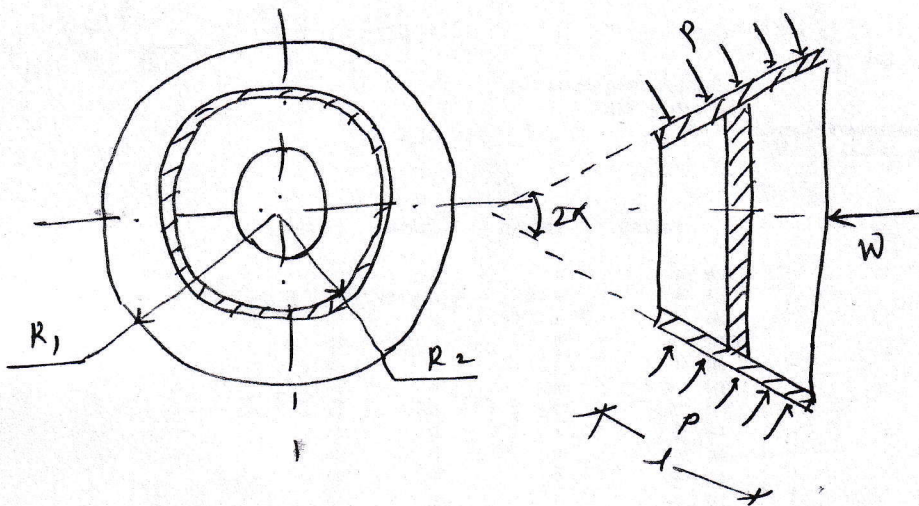


Fig:-

2 marks

1) Uniform pressure theory

$$T = \frac{2}{3} \mu W \left[\frac{R_1^3 - R_2^3}{R_1^2 - R_2^2} \right] \cos \alpha$$

2 marks

2) Uniform wear theory

$$T = \frac{1}{2} \mu W (R_1 + R_2) \cos \alpha$$

2 marks

b] $R_1 = 0.22 \text{ m}$

$R_2 = 0.177 \text{ m}$

— 2 marks

$W = 714.42 \text{ N}$ — 2 marks

c] centrifugal clutch:- Fig — 2 marks

Explanation — 2 marks